**H ∞ active anti-roll bar control to prevent rollover of heavy vehicles: a robustness analysis**

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Abstract: Rollover of heavy vehicle is an important road safety problem world-wide. Although rollovers are relatively rare events, they are usually deadly accidents when they occur. In order to improve roll stability, most of modern heavy vehicles are equipped with passive anti-roll bars to reduce roll motion during cornering or riding on uneven roads. This paper proposes an $H_{\infty}$ approach to design active anti-rollover bars using the yaw-roll model of a single unit heavy vehicle. The control signals are the torques generated by the actuators at the front and rear axles. Simulation results in both frequency and time domains are provided to compare two different contexts: passive anti-roll bars and $H_{\infty}$ active anti-roll bars. It is shown that the use of two $H_{\infty}$ active (front and rear) anti-roll bars drastically improves the roll stability of the single unit heavy vehicle to prevent rollover.

Keywords: Vehicle dynamics, Active anti-roll bar control, Rollover, Roll stability, $H_{\infty}$ control, $\mu$-analysis.

1. INTRODUCTION

1.1 Context

The rollover is a very serious problem for heavy vehicle safety, which can result in large financial and environmental consequences. The aim of preventing rollovers is to provide the vehicle with an ability to resist overturning moments generated during cornering and lane changing to avoid obstacles.

In order to improve roll stability, most of modern heavy vehicles are equipped with passive anti-roll bars to reduce roll motion. The passive anti-roll bar force is a function of the differences between right and left suspensions deflections. The force is applied by the bar on each side of the vehicle so that the left force has the same magnitude but the opposite direction than the right one. The passive anti-roll bar has the advantages to reduce the body roll acceleration and roll angle during single wheel lifting and cornering maneuvers. However, the passive anti-roll bar also has drawbacks. During cornering maneuvers, anti-roll bar transfers the vertical forces of one side of suspension to the other one, creating therefore a moment against lateral force.

In order to overcome the drawbacks of the passive anti-roll bar systems, several schemes with possible active intervention into the vehicle dynamics have been proposed. One of these methods employs active anti-roll bars, that is, a pair of hydraulic actuators which generate a stabilizing moment to balance the overturning moment. Lateral acceleration makes vehicles with conventional passive suspension tilt out of corners. The center of the sprung mass shifts outboard of the vehicle centerline, which creates a destabilizing moment that reduces roll stability. The lateral load response is reduced by active anti-roll bars which generate a stabilizing moment to counterbalance the overturning moment in such a way that the control torque leans the vehicle into the corners (see Sampson and Cebon (2003), Gaspar et al. (2004)). Other methods can be used (active steering, electronic brake mechanism,...) but they are beyond the scope of this paper.

The disadvantage of the active anti-roll bars is that the maximum stabilizing moment is limited physically by the relative roll angle between the body and the axle (Sampson and Cebon (2002)).

1.2 Related works

Some of the control methods applied for active anti-roll bar control on heavy vehicle are briefly presented below:

a- Optimal control: Sampson et al (see Sampson and Cebon (1998)). Sampson and Cebon (2002)) have proposed a state feedback controller which was designed by finding an optimal controller based on a linear quadratic regulator (LQR) for single unit and articulated heavy vehicles. They used the control torques acting between the axle groups and the sprung mass as the input control signal.

The LQR has been also applied to the integrated model including an electronic servo-valve hydraulic damper model and a yaw-roll model of a single unit heavy vehicle. The input control signal is the input current of the electronic servo-valve (Vu et al., 2016).

b- Neural network control: Boada et al. (2007) have proposed a reinforcement learning algorithm using neural networks to improve the roll stability for a single unit heavy vehicle. The input control signals are the torques at the axles. However this kind of approach is not suitable for embedded control.

c- Robust control (LPV): Gaspar et al (see Gaspar et al. (2005a), Gaspar et al. (2004) and Gaspar et al. (2005b)) have applied Linear Parameter Varying (LPV) for the active anti-roll bar combined with an active brake control on the single unit heavy vehicle. They also used a Fault Detection and Identification (FDI) filter, which identifies different actuator failures. The forward velocity is considered as the varying parameter.
1.3 Paper contribution

Based on the model presented in (Gaspar et al. (2004)), this paper proposes an $H_{\infty}$ control method for active anti-roll bar, and focuses on the uncertainties due to the vehicle forward velocity and the sprung mass variations. Hence the following contributions are brought:

- We design a $H_{\infty}$ robust controller for active anti-roll bar system on the single unit heavy vehicle. The aim is to maximize the roll stability to prevent rollover of heavy vehicles. The normalized load transfer and the limitation of the torque generated by actuators in various maneuver situations are considered.
- Performance analysis made in frequency domain shows that the $H_{\infty}$ active anti-roll bar control drastically reduces the normalized load transfer compared to the passive anti-roll bar. It also shows that the $H_{\infty}$ active anti-roll bar control is robust w.r.t. the forward velocity and the sprung mass variation. The robust stability analysis of the designed controller is performed using the $\mu$-analysis method.
- In time domain, we use a double lane change as the heavy vehicle maneuver. The simulation results indicate that the Root Mean Square (RMS) of the $H_{\infty}$ active anti-roll bar control have dropped from 15% to 50% compared to the passive anti-roll bar with all of the forward velocity considered in interval from 50Km/h to 110Km/h.

The paper is organised as follows: Section 2 gives the model of a single unit heavy vehicle. Section 3 presents the design of the passive anti-roll bar. Section 4 gives the $H_{\infty}$ robust control synthesis to prevent rollover of heavy vehicles. Section 5 illustrates the robustness analysis in the frequency domain using the $\mu$-tool. Section 6 illustrates the simulations in time domain. Finally, some conclusions are drawn in section 7.

2. SINGLE UNIT HEAVY VEHICLE MODEL

Fig 1 illustrates the combined yaw-roll dynamics of the vehicle modelled by a three-body system, in which $m_s$ is the sprung mass, $m_{uf}$ the unsprung mass at the front including the front wheels and axle, and $m_{ur}$ the unsprung mass at the rear with the rear wheels and axle. The parameters and variables of the yaw-roll model are shown in the table 1.

In the vehicle modelling, the differential equations of motion of the yaw-roll dynamics of the single unit vehicle, i.e. the lateral dynamics, the yaw moment, the roll moment of the sprung mass, the roll moment of the front and the rear unsprung masses, are formalized in the equations (1):

$$
egin{align*}
\dot{mv^2}(\beta + \psi) - m_vh^2\psi &= F_{yf} + F_{yr} \\
-1m_vh^2\dot{\psi} &= F_{yf} + F_{yr} \\
(1 + m_vh^2)^2\dot{\beta} - 1m_vh^2\psi &= m_sgh^2b_m(\beta + \psi) \\
-k_1(\phi - \phi_f) - b_1(\phi - \phi_{ef}) + M_{ARf} + U_f \\
-k_2(\phi - \phi_r) - b_2(\phi - \phi_{er}) + M_{ARr} + U_r \\
-rF_{yf} &= m_{uf}g\phi + l^2_m + m_{ur}g\phi + m_vh^2(\beta + \psi) \\
+k_1(\phi - \phi_f) + b_1(\phi - \phi_f) + M_{ARf} + U_f \\
-rF_{yr} &= m_{ur}gh_{ur}\phi_f + l^2_m - k_1\phi_f \\
+k_2(\phi - \phi_r) + b_2(\phi - \phi_{er}) + M_{ARr} + U_r
\end{align*}
$$

(1)

In (1) the lateral tire forces $F_{yf}$, in the direction of velocity at the wheel ground contact points are modelled by a linear stiffness as:

$$
egin{align*}
F_{yf} &= \mu C_{t}\alpha_f \\
F_{yr} &= \mu C_{t}\alpha_r
\end{align*}
$$

with tire side slip angles:

$$
\left\{ \begin{array}{l}
\alpha_f = -\beta + \delta_f - \frac{l_f\psi}{v} \\
\alpha_r = -\beta + \frac{l_r\psi}{v}
\end{array} \right.
$$

(3)

Let us now detail how the moment $M_{ARf}$ and $M_{ARr}$ in (1) are computed. When the vertical displacements of the left and the right wheels differ, the passive anti-roll bar with a rotational stiffness $k_{Ao}$ creates an anti-roll moment, resulting in the anti-roll force $F_{Au}$, see Figure 2, acting on the unsprung mass as:

$$
F_{Au} = -F_{Au'} = k_{Ao}(\Delta Z_{Ar} - \Delta Z_{Al})
$$

(4)

and the anti-roll force $F_{As}$ acting on the sprung mass is:

$$
F_{As} = -F_{As'} = F_{Au'}l_A = k_{As}(\Delta Z_{Ar} - \Delta Z_{Al})
$$

(5)

where $\Delta Z_{Ar}$ are the displacements of the connection point between the anti-roll bars and the wheels, $l_A$ is half the distance of the two suspensions, $l_P$ is half the distance of the chassis, $c$ is the length of the anti-roll bars’s arm, $k_{Au}$ and $k_{As}$ are the modified rotational stiffness corresponding to the unsprung and sprung mass, respectively:

$$
k_{Au} = k_{Ao}\frac{1}{c^2}
$$

and

$$
k_{As} = k_{Ao}\frac{l_A}{l_Pc^2}
$$

(6)

The moment of passive anti-roll bar impacts the unsprung and sprung masses at the front axle as follows:

<table>
<thead>
<tr>
<th>Symbols</th>
<th>Description</th>
<th>Value</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$m_s$</td>
<td>Sprung mass</td>
<td>12487</td>
<td>kg</td>
</tr>
<tr>
<td>$m_{uf}$</td>
<td>Unsprung mass on the front axle</td>
<td>706</td>
<td>kg</td>
</tr>
<tr>
<td>$m_{ur}$</td>
<td>Unsprung mass on the rear axle</td>
<td>1000</td>
<td>kg</td>
</tr>
<tr>
<td>$m$</td>
<td>The total vehicle mass</td>
<td>14193</td>
<td>kg</td>
</tr>
<tr>
<td>$v$</td>
<td>Forward velocity</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$r$</td>
<td>Height of CG of unsprung mass from ground</td>
<td>0.53</td>
<td>m</td>
</tr>
<tr>
<td>$h$</td>
<td>Height of CG of sprung mass from roll axis</td>
<td>1.15</td>
<td>m</td>
</tr>
<tr>
<td>$\phi$</td>
<td>Yaw rate</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\beta$</td>
<td>Side-slip angle at center of mass</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\psi$</td>
<td>Heading angle</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\alpha_f$</td>
<td>Lateral acceleration</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\alpha_r$</td>
<td>Side slip angle</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\phi_s$</td>
<td>Sprung mass roll angle</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\phi_i$</td>
<td>Unsprung mass roll angle</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\delta_f$</td>
<td>Steering angle</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$u_i$</td>
<td>Control current</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$C_f$</td>
<td>Tire cornering stiffness on the front axle</td>
<td>582</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$C_r$</td>
<td>Tire cornering stiffness on the rear axle</td>
<td>783</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$k_{zf}$</td>
<td>Suspension roll stiffness on the front axle</td>
<td>380</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$k_{zr}$</td>
<td>Suspension roll stiffness on the rear axle</td>
<td>684</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$b_f$</td>
<td>Suspension roll damping on the front axle</td>
<td>10</td>
<td>kNs/deg</td>
</tr>
<tr>
<td>$b_r$</td>
<td>Suspension roll damping on the rear axle</td>
<td>10</td>
<td>kNs/deg</td>
</tr>
<tr>
<td>$k_{zf}$</td>
<td>Tire roll stiffness on the front axle</td>
<td>2060</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$k_{zr}$</td>
<td>Tire roll stiffness on the rear axle</td>
<td>3337</td>
<td>kN/deg</td>
</tr>
<tr>
<td>$l_{xs}$</td>
<td>Roll moment of inertia of sprung mass</td>
<td>24201</td>
<td>kNm^2</td>
</tr>
<tr>
<td>$I_{xz}$</td>
<td>Yaw-roll product of inertia of sprung mass</td>
<td>4200</td>
<td>kNm^2</td>
</tr>
<tr>
<td>$l_{zc}$</td>
<td>Yaw moment of inertia of sprung mass</td>
<td>34917</td>
<td>kNm^2</td>
</tr>
<tr>
<td>$l_f$</td>
<td>Length of the front axle from the CG</td>
<td>1.95</td>
<td>m</td>
</tr>
<tr>
<td>$l_r$</td>
<td>Length of the rear axle from the CG</td>
<td>1.54</td>
<td>m</td>
</tr>
<tr>
<td>$l_w$</td>
<td>Half of the vehicle width</td>
<td>0.93</td>
<td>m</td>
</tr>
<tr>
<td>$\mu$</td>
<td>Road adhesion coefficient</td>
<td>1</td>
<td>-</td>
</tr>
</tbody>
</table>
The moment of passive anti-roll bar impacts the unsprung and sprung masses at the rear axle as follows:

\[
M_{AR} = 4k AO f_t^\phi - 4k AO f_c^\phi u f_t \tag{7}
\]

The design of an anti-roll bar actually aims at obtaining the required anti-roll stiffness \( k_{AO} \) that improves the vehicle stability and handling performances without exceeding the mechanical limitations of the bar material (Bharane et al. (2014) for general information about torsion bars and their manufacturing processing in Spring Design Manual). Anti-roll bars are special cases of torsion bars. Some useful formulae to calculate the torsional stiffness of anti-roll bars and deflection at the end point of the bar under a given loading, are provided in the manual. However, the formulations can only be applied to the bars with standard shapes (simple, torsion bar shaped anti-roll bars). The applicable geometry is shown in Figure 3.

Using the previous equation, the single unit heavy vehicle is represented by the linear system in the state space form (9):

\[
\begin{align*}
\dot{x} &= Ax + Bu \\
y &= Cx
\end{align*}
\]

where the state vector:

\[
x = \begin{bmatrix} \beta & \dot{\psi} & \phi & \phi_u & \phi_v \end{bmatrix}^T
\]

the input vector:

\[
u = \begin{bmatrix} \delta_f & U_f & U_r \end{bmatrix}^T
\]

and the output vector:

\[
y = \begin{bmatrix} \beta & \dot{\psi} & \phi & \phi_u & \phi_v \end{bmatrix}^T
\]

Remark: Note that matrix \( A \) mainly depends on the forward velocity (\( V \)) and the sprung mass (\( m_s \)). The design of \( H_\infty \) controller will be done considering the nominal matrix \( A \) and the effect of uncertainties will be analysed in section 5.

3. DESIGN OF A PASSIVE ANTI-ROLL BAR

The load \( P \) is applied at point \( A \), inward to or outward from plane of the page. The roll stiffness of such a bar can be calculated as:

\[
k_{AO} = \frac{PL^2}{2f_A^2} \tag{10}
\]

with \( f_A \) - Deflection of point \( A \):

\[
f_A = \frac{P}{3EI} \left[ (a - a_1)^3 + \frac{L}{2} (a + b)^2 + 4f_2^3 (b + c) \right] \tag{11}
\]

\( L \) - Half track length of anti-roll bar:

\[
L = a + b + c \tag{12}
\]

and \( I \) - Moment of inertia of anti-roll bar:

\[
I = \frac{\pi D^4}{64} \tag{13}
\]
where $D$ is the outer diameter and $E$ the young’s modulus of material. The material of anti-roll bar is issued from AISI 1065, $E = 2060000\text{MPa}$ (see Bharane et al. (2014)). The outer diameter of the anti-roll bar on the front axle $D_f = 32\text{mm}$ (Vu et al., 2016), the torsional stiffness of the anti-roll bar at the front axle is:

$$k_{AO_f} = 10730 \, (\text{Nm/rad})$$

The outer diameter of the anti-roll bar on the rear axle $D_r = 34\text{mm}$ (Vu et al., 2016), the torsional stiffness of the anti-roll bar at the rear axle is:

$$k_{AO_r} = 15480 \, (\text{Nm/rad})$$

4. $H_\infty$ ROBUST CONTROL SYNTHESIS TO PREVENT ROLLOVER OF HEAVY VEHICLES

4.1 Control objective, problem statement

The objective of the active anti-roll bar control system is to maximize the roll stability of the vehicle. The rollover is caused by the high lateral inertial force generated by lateral acceleration. If the position of the center of gravity is high or the forward velocity of the vehicle is larger than allowed at a given steering angle, the resulting lateral acceleration is also large and might initiate a rollover. An imminent rollover can be detected if the calculated normalized load transfer reaches 1 (or –1), as explained below.

First, the lateral load transfer can be given by:

$$\Delta F_z = k_w \phi_u \frac{l_w}{I_w}$$

where $k_w$ is the stiffness of tire, $\phi_u$ the roll angle of the unsprung mass and $l_w$ the half of vehicle’s width. Then, the lateral load transfer can be normalized w.r.t. the total axle load $F_z$ as follows:

$$R = \frac{\Delta F_z}{F_z}$$

The normalized load transfer $R$ value corresponds to the largest possible load transfer. When $R = \pm 1$, the inner wheel in the bend lifts off.

The roll stability is achieved by limiting the normalized load transfer within the levels corresponding to wheel lift-off. Specifically, the load transfer can be minimized to increase the inward lean of the vehicle. The center of mass shifts laterally from the nominal center line of the vehicle to provide a stabilizing effect. While attempting to minimize the load transfer, it is also necessary to constrain the roll angles between the sprung and unsprung masses ($\phi - \phi_u$) so that they stay within the limits of the suspension travel ((7 – 8deg) see Gaspar et al. (2004)).

By minimizing a suitably weighted version of (19) the control aim is achieved, as presented below.

4.2 Background on $H_\infty$ control

The interested reader may refer to (Skogestad and Postlethwaite, 2001), (Scherer and Weiland, 2005) for further explanations on $H_\infty$ control design.

The $H_\infty$ control problem is formulated according to the generalized control structure shown in Fig 4.

$$\begin{align*}
\begin{bmatrix} z \\ y \end{bmatrix} &= \begin{bmatrix} P_{11}(s) & P_{12}(s) \\ P_{21}(s) & P_{22}(s) \end{bmatrix} \begin{bmatrix} d \\ u \end{bmatrix} \\
\begin{bmatrix} d \\ u \end{bmatrix} &= \begin{bmatrix} K(s) \end{bmatrix}y 
\end{align*}$$

(16)

and

(17)

which yields

$$\frac{z}{d} = \mathcal{F}(P, K) := [P_{11} + P_{12}K[I - P_{22}K]^{-1}P_{21}]$$

(18)

The aim is to design a controller $K$ that reduces the signal transmission path from disturbances $d$ to performance outputs $z$ and also stabilizes the closed-loop system. This problem aims at finding $K$ which minimizes $\gamma$ such that

$$\|\mathcal{F}(P, K)\|_{H_\infty} < \gamma$$

(19)

By minimizing a suitably weighted version of (19) the control aim is achieved, as presented below.

4.3 $H_\infty$ control synthesis for the active anti-roll bar of the single unit heavy vehicle model

According to Fig 5 the concatenation of the linear model (9) with performance weighting functions lead to the state space representation of $P(s)$:

$$\begin{bmatrix} X \\ Z \\ Y \end{bmatrix} = \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix} \begin{bmatrix} X \\ W \\ U \end{bmatrix}$$

(20)

with the exogenous input (disturbance):

$$W = \begin{bmatrix} d & n_1 & n_2 \end{bmatrix}$$
the control input:

$$U = \left[ U_f, U_r \right]^T$$

where $U_f$ is the torque at the front axle, $U_r$ is the torque at the rear axle.

the performance output vector:

$$Z = \left[ e_1, e_2, e_3, e_4, e_5 \right]^T$$

the measured output vector:

$$Y = \left[ a_1, \phi \right]^T$$

and $A$, $B_1$, $B_2$, $C_1$, $D_{11}$, $D_{12}$, $C_2$, $D_{21}$, $D_{22}$ are model matrices of appropriate dimensions.

In $H_{\infty}$ control the selection of the weighting functions is a key step that is to be handled using the knowledge of the engineers concerning the system behavior and characteristics. The weighting functions of Fig 5 are given here after.

The input scaling weight $W_i$ normalizes the steering angle to the maximum expected command and is selected as follows:

$$W_i = \pi/180$$

This value corresponds to a 1° steering angle command.

The weighting functions $W_{n1}$ and $W_{n2}$ are selected as:

$$W_{n1} = W_{n2} = 0.01$$

which accounts for small sensor noise models in the control design. The noise weights are chosen 0.01$(m/s^2)$ for the lateral acceleration and 0.01$(/sec)$ for the derivative of roll angle $\phi$ (see (Gaspar et al., 2004)). Other low pass filters could be selected.

The weighting functions $W_2$ represent the performance outputs ($W_{z1}$, $W_{z2}$, $W_{z3}$, $W_{z4}$ and $W_{z5}$). The purpose of the weighting functions is to keep small the control inputs, normalized load transfers and the lateral acceleration over the desired frequency range. The weighting functions chosen for performance outputs can be considered as penalty functions, that is, weights should be large in the frequency range where small signals are desired and small where larger performance outputs can be tolerated.

The weighting functions $W_{z1}$ and $W_{z2}$ are chosen as:

$$W_{z1} = 1/1.5 \times 10^5, \quad W_{z2} = 1/2 \times 10^5$$

which correspond to the front and rear control torques generated by active anti-roll bars.

The weighting functions $W_{z3}$ and $W_{z4}$ are selected as:

$$W_{z3} = W_{z4} = 1$$

which means that the maximal gain of the normalized load transfers can be 1 in the frequency domain for front and rear axles.

The weighting function $W_{z5}$ is selected as:

$$W_{z5} = \frac{(s/2000 + 50)}{(s/0.01 + 0.01)} \quad (21)$$

Here, the weighting function $W_{z5}$ corresponds to a design that avoids the rollover situation with the bandwidth of the driver in frequency range up to more than $4rad/s$. This weighting function will minimize directly the lateral acceleration when it reaches the critical value to avoid the rollover.

4.4 Frequency domain analysis with nominal value

The limited bandwidth of the driver must be considered up to $4rad/s$ to identify any resonances in the response that may be excited by the driver (see Gaspar et al. (2004) and Sampson (2000)). Therefore, it is necessary to consider the behavior of the heavy vehicle in a wider frequency range. In this section, the frequency response of heavy vehicle is shown in the nominal parameters case.

The nominal parameters of single unit heavy vehicle considered include the sprung mass $m_s = 12487kg$, the forward velocity $V$ at 70km/h and the road adhesion coefficient $\mu = 1$. The frequency responses of the single unit heavy vehicle are shown in Fig 6.

Fig 6a shows the normalized load transfer at the front axle $R_f$ due to steering angle $\delta_f$. It shows that the $H_{\infty}$ active anti-roll bar controller reduces the normalized load transfer (about $3dB$) in frequency range up to $7.0rad/s$ compared to the passive anti-roll bar. Fig 6b shows the normalized load transfer at the rear axle $R_r$. It indicate that the $H_{\infty}$ active anti-roll bar controller reduces the normalized load transfer at the rear axle (about $4.5dB$) throughout the main frequency range. As a consequence, the $H_{\infty}$ active anti-roll bar can improve the roll stability to prevent rollover.

Fig 6a,b also indicate that the normalized load transfers build up more quickly at the rear axle than at the front axle with the cases of the passive anti-roll bar as well as the $H_{\infty}$ active anti-roll bar. This is consistent with the previous results (see (Sampson, 2000)).

The simulation results in Fig 6a,b fulfil the main objective of designing $H_{\infty}$ active anti-roll bar control system which is to minimize the normalized load transfer to prevent rollover of heavy vehicle.

Fig 6c,d show the control inputs of the $H_{\infty}$ active anti-roll bar which are the torque at the front ($U_f$) and the rear axle ($U_r$). It indicates that the torque at the rear axle is always greater than that of front axle about $5dB$ throughout the main frequency range. This ensures that the normalised load transfer at rear axle is more minimized than that at the front axle. This explains why the normalised load transfers at the front and rear axles for the passive anti-roll bar are $23dB$ and $25dB$, respectively. Meanwhile, the normalised load transfers at the front and rear axles for the $H_{\infty}$ active anti-roll bar control equal approximately $20dB$.

5. ROBUSTNESS ANALYSIS IN THE FREQUENCY DOMAIN USING THE $\mu$-TOOL

5.1 Robust stability and performance analysis

A control system is robust if it is insensitive to differences between the actual real system and the model used to design the controller. Let us recall that, in addition to nominal stability and performance, the objectives of any control system include: Robust Stability (RS). The system is stable for all perturbed plants around the nominal model up to the worst-case model uncertainty.

Robust Performance (RP). The system satisfies the performance specifications for all perturbed plants around the nominal model up to the worst-case model uncertainty.

The current application is concerned by parametric uncertainties. In particular, the forward velocity and the sprung mass are assumed to be badly known. In the considered yaw-roll model (1), the forward velocity is the most varying parameter. The other parameters variations come from the industrial manufacturing only. The uncertainties are therefore represented as:

$$V = V(1 + p_V\delta_V), \quad p_V = 57.14\%, \quad \delta_V \in [-1:1]$$

$$m_s = m_s(1 + p_m\delta_m), \quad p_m = 30\%, \quad \delta_m \in [-1:1]$$

Using ad hoc LFT representations of the parametric uncertainties, we can pull out the perturbations in a diagonal block as:

$$\Delta_r = diag(\delta_V I, \delta_m I_m)$$
The starting point of the robustness analysis is the block-diagonal representation of the uncertainties:
\[ \Delta = \text{diag}(\Delta_1, \ldots, \Delta_q, \Delta_r) \]
where \( \Delta_i(s), \Delta_r(s) \) represent full block complex uncertainties, \( \delta_i(s), \delta_r(s) \) real parametric uncertainties, and \( \epsilon_i(s), \epsilon_r(s) \) complex parametric uncertainties.

Taking into account the uncertainties leads to the following General Control Configuration given in Fig 7, where \( \Delta \in A \).

Here, only real parametric uncertainties (\( \Delta_r \)) are considered for RS analysis. RP analysis also needs a fictive full block complex uncertainty, as shown in Fig 8.

\[ T_{ru}(s) = N_{22}(s) + N_{21}(s)\Delta(s)(I - N_{11}(s))^{-1}N_{12}(s) \]  (22)

Note that in (22), \( N_{22}(s) = N_{rw} \) is the nominal closed-loop transfer matrix. If it is stable, the instability in (22) may only come from \( (I - N_{11}(s))^{-1} \).

As we consider structured uncertainties, a \( \mu \)-analysis is used for the RS and RP analysis. First the structured singular value is defined as:
\[ \mu(A):= \min|\mathcal{P}(\Delta): \Delta \in A, \det(I - \Delta M) = 0| \]

For RS, we determine how large \( \Delta \) (in the sense of \( H_\infty \)) can be without destabilizing the feedback system. From (22), the feedback system becomes unstable if \( \det(I - N_{11}(s)) = 0 \) for some \( s \in \mathbb{C}, \mathcal{R}(s) \geq 0 \). The following theorem is used.

Theorem 1. (Skogestad and Postlethwaite, 2001) Assume that the nominal system \( N_{rw} \) and the perturbations \( \Delta \) are stable. Then the feedback system is stable for all allowed perturbations \( \Delta \) such that \( \|\Delta(s)\|_{\infty} < 1/\beta \) if and only if \( \forall \omega \in \mathbb{R}, \mu(\Delta(s)) \leq \beta \).

Assuming nominal stability, RS and RP analysis for structured uncertainties are therefore such that:
\[ \text{RS} \Leftrightarrow \mu_{\Delta}(N_{11}) < 1, \forall \omega \]  (23)
\[ \text{RP} \Leftrightarrow \mu_{\Delta}(N) < 1, \forall \omega, \Delta = \begin{bmatrix} \Delta_f & 0 \\ 0 & \Delta_r \end{bmatrix} \]  (24)

Finally, let us remark that the structured singular value cannot be explicitly determined. The method consists then in calculating an upper bound and a lower bound, as close as possible to \( \mu \).

B. Robust stability for \( H_\infty \) active anti-roll bar control

Applying the theorem 1, an upper bound of \( \mu \) for RS and RP is given in Fig 9 and Fig 10. As \( \mu_{\Delta}(N_{11}) \leq 0.6023 \), RS is satisfied. Hence the \( H_\infty \) controller keeps stability for the considered uncertainties. Moreover, this means that the closed-loop system remains stable for larger uncertainties, i.e.:
\[ V = 70\text{Km/h} \pm (57.14/0.6023)\% = 70\text{Km/h} \pm 94.87\% \]
\[ m_r = 12487\text{kg} \pm (30/0.6023)\% = 12487\text{kg} \pm 49.81\% \]

On the other hand, as \( \mu_{\Delta}(N) < 1 \), we can conclude that the Robust Performance is satisfied in this uncertainty case.
In this section, the robustness of the $H\infty$ active anti-roll bar control is evaluated by changing the forward velocity from $50\text{Km/h}$ to $110\text{Km/h}$. Fig 11a,b show the normalized load transfer at the front axle $R_f$ and at rear axle $R_r$ due to steering angle $\delta_f$ with the forward velocity variation. When compared to the passive anti-roll bar, One sees that the normalized load transfers at the front axle $R_f$ and at rear axle $R_r$ due to steering angle $\delta_f$.
in case of the $H_{\infty}$ active anti-roll bar control have been reduced in frequency range up to 7.0rad/s. Meanwhile the normalized load transfers at the rear axle $R_r$ have been reduced throughout the main frequency range. The reduction of the normalized load transfer at the front and at the rear axles in desired frequency range improves then the roll stability which prevents the rollover of the single unit heavy vehicle. Fig 11c,d show the control inputs $(U_f, U_r)$ of the $H_{\infty}$ active anti-roll bar at two axle. The torque at the rear axle is always greater than that of front axle throughout the main of the frequency range when the forward velocity varies from $50\text{Km/h}$ to $110\text{Km/h}$. From the simulation results above, we can claim that the $H_{\infty}$ active anti-roll bar control is robust w.r.t. the forward velocity variation.

6. SIMULATIONS IN TIME DOMAIN

In this section, the considered vehicle maneuver is a double lane change for overtaking. The lane used to overtake another vehicle is almost always a passing lane further from the road shoulder. Figure 12a shows the steering angle $\delta$ corresponding to a double lane change. The forward velocity is considered constant from $50\text{Km/h}$ to $110\text{Km/h}$. Fig 12c,d show the normalized load transfers at the front and rear axles, respectively. With the $H_{\infty}$ active anti-roll bar, the values of normalized load transfer at the front and rear axles are always within $\pm1$, while the normalized load transfer at rear axle of the passive anti-roll bar exceeds $\pm1$ when the forward velocity $V = 110\text{Km/h}$. At this velocity, the wheels of vehicle lift on, leading to rollover. Fig 12b shows the torques at front and rear axles. They increase with the forward velocity. Fig 13 summarizes the performance assessment of the roll stability of the single unit heavy vehicle using the $H_{\infty}$ active anti-roll bar control. The Root Mean Squares (RMS) of the normalized load transfers and the roll angles of suspension are compared to that of the passive anti-roll bar (corresponding to 100\%).

$$\frac{\text{RMS(active)}}{\text{RMS(passive)}} = 100\%$$ (25)

The RMS of the $H_{\infty}$ active anti-roll bar control have been reduced from 15% to 50% compared to the passive anti-roll bar. It also shows that the $H_{\infty}$ active anti-roll bar control has reduced a lot of the RMS values when the forward velocity varies from $70\text{Km/h}$ to $100\text{Km/h}$. This is also the "danger" zone of the forward velocity of heavy vehicle when the vehicle maneuver is a double lane change to overtake.

7. CONCLUSION

In this paper, the Yaw - Roll model of a single unit heavy vehicle including active anti-roll bar systems at two axles is used. A linear $H_{\infty}$ control scheme is developed to maximize its roll stability in order to prevent rollover. The normalized load transfers and the limitations of the torque generated by actuators are considered.

Simulation results both in frequency and time domains demonstrate that the $H_{\infty}$ active anti-roll bar control completely reduces the normalized load transfers and the roll angles of suspension compared to the passive anti-roll bar. A $\mu$-analysis confirms that the closed-loop system remains stable for larger uncertainties with the forward velocity $V = 70\text{Km/h} \pm 94.87\%$ and the sprung mass $m_s = 12487\text{kg} \pm 49.81\%$. Even if a LTI controller seems to performs reasonably well here, the comparison with an LPV controller (scheduled by the vehicle velocity) will be of interest.

REFERENCES


Fig. 13. RMS of the $H_{\infty}$ active anti-roll bar control compared to the passive anti-roll bar (100%).